

Upstream Passage of Potamodromous Cyprinids Over Small Weirs: the Influence of Key-Hydraulic Parameters

Journal:	<i>Journal of Ecohydraulics</i>
Manuscript ID	TJoE-2016-0016.R1
Manuscript Type:	Original Article
Date Submitted by the Author:	24-Aug-2016
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Keywords:	river connectivity, small weirs, potamodromous cyprinid species, upstream migration, ecohydraulics
Abstract:	The presence of small weirs, far more numerous than dams, has increased habitat fragmentation on rivers worldwide. This study aims to evaluate the upstream passage performance of a potamodromous cyprinid, the Iberian barbel (<i>Luciobarbus bocagei</i>), over an experimental broad-crested weir by varying key-hydraulic parameters. Fish passage success was studied for different combinations of waterfall height (Δh), plunge pool depth (D) and flow discharge (Q). The flow pattern downstream of the weir was characterized with a 3D Acoustic Doppler Velocimeter, to assess the effects of hydrodynamics on fish behaviour. Results showed that D , Δh , and their

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	<p>interaction $D \times \Delta h$ (PerMANOVA, $p < 0.01$), as well as Q (Kruskal–Wallis $H = 10.95$; 3 d.f.; $p = 0.01$) were significantly correlated with the number of successful upstream fish passages. However, counter-intuitively, higher fish passage success did not occur at combinations of lower Δh and Q, and higher D. Therefore, upstream fish passage appears to be a complex phenomenon, which is strongly dependent on the hydraulic environment that is produced by the interaction of these parameters. The outcomes of this work will help engineers and biologists to establish design criteria for requalification of small barriers in order to improve fish passage and habitat connectivity.</p>

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5 2 **Influence of Key-Hydraulic Parameters**
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51 Upstream Passage of Potamodromous Cyprinids Over Small Weirs: the 52 Influence of Key-Hydraulic Parameters

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54 The presence of small weirs, far more numerous than dams, has increased habitat
55 fragmentation on rivers worldwide. This study aims to evaluate the upstream passage
56 performance of a potamodromous cyprinid, the Iberian barbel (*Luciobarbus bocagei*), over an
57 experimental broad-crested weir by varying key-hydraulic parameters. Fish passage success
58 was studied for different combinations of waterfall height (Δh), plunge pool depth (D) and
59 flow discharge (Q). The flow pattern downstream of the weir was characterized with a 3D
60 Acoustic Doppler Velocimeter, to assess the effects of hydrodynamics on fish behaviour.
61 Results showed that D, Δh , and their interaction $D \times \Delta h$ (PerMANOVA, $p < 0.01$), as well as Q
62 (Kruskal–Wallis $H = 10.95$; 3 *df.*; $p = 0.01$) were significantly correlated with the number of
63 successful upstream fish passages. However, counter-intuitively, higher fish passage success
64 did not occur at combinations of lower Δh and Q, and higher D. Therefore, upstream fish
65 passage appears to be a complex phenomenon, which is strongly dependent on the hydraulic
66 environment that is produced by the interaction of these parameters. The outcomes of this
67 work will help engineers and biologists to establish design criteria for requalification of small
68 barriers in order to improve fish passage and habitat connectivity.

69
70 **Keywords:** river connectivity; small weirs; potamodromous cyprinid species; upstream
71 migration; ecohydraulic

73 Introduction

74 River fragmentation caused by the presence of instream obstacles has been considered one of
75 the main threats to the sustainability of fish populations, being responsible for the decline or
76 even extinction of populations through demographic, environmental and genetic stochasticity

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3 77 (Aarts et al. 2003; Nilsson et al. 2005). Nevertheless, barriers to fish migration occur not only
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5 78 through the presence of large dams and small hydropower plants, which have recently
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7 79 increased as result of the promotion of renewable forms of energy (Santos et al. 2006; Crook
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10 80 et al. 2015), but also mainly through other artificial obstacles such as small weirs (Lucas and
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12 81 Baras 2001). These obstacles, that are in general less than 5 m in height (ONEMA 2010; Solà
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14 82 et al. 2011) and are considered to be 2-4 orders of magnitude far more numerous than large
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16 83 structures (Lucas et al. 2009), alter the velocity patterns and the water depth, creating vertical
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18 84 drops that change the hydrodynamics of aquatic systems and may prevent the movement of
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20 85 fish species and hence their access to spawning, feeding and rearing areas (Leaniz 2008;
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22 86 Branco et al. 2012). However, compared with large regulated schemes, the effects of small
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24 87 weirs and natural obstacles are much less well quantified, thus deserving greater attention not
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26 88 only due to their much higher numbers (in the Portuguese Tagus basin alone, there are more
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28 89 than 2000 small weirs), but also because they can have a significant effect on fish movements,
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30 90 thereby potentially causing changes in the composition and structure of assemblages (Ovidio
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32 91 and Philippart 2002; Poulet 2007; Ordeix et al. 2011). This is in accordance with recent
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34 92 research lines and European projects, which emphasize the need for additional scientific
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36 93 studies to address the impact of small barriers on fish passage success (Harford and
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38 94 McLaughlin 2007).

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43 95 Previous studies on the upstream passage of small weirs have been mainly focused on
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45 96 salmonid species (e.g. Brandt et al. 2005; Lauritzen et al. 2005; Kondratieff and Myrick 2006;
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47 97 Kemp et al. 2006; Ovidio et al. 2007) and have shown that fish capacity to negotiate these
48
49 98 obstacles is not only related with their swimming and jumping performance, but also with
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51 99 obstacle design and hydrodynamic conditions downstream of the weir (e.g. waterfall height,
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53 100 weir slope, plunge pool depth, flow discharge, turbulence). In this respect, the plunge pool
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55 101 depth (water depth below the weir) and waterfall height (distance from the plunge pool
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3 102 surface to the top of the weir crest) emerged as the two most important variables influencing
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5 103 fish movements in broad-crested weirs, which are typically constructed with a vertical
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7 104 downstream face from reinforced concrete, spanning the full width of the river channel
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10 105 (Baudoin et al. 2014).

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12 106 The effect of plunge pool depth and waterfall height on the successful passage of fish
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14 107 has been investigated in order to improve knowledge on more effective upstream passage of
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16 108 fish. For example, analysing the ratio of plunge pool depth/waterfall height, Stuart (1962)
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18 109 found that for brown trout (*Salmo trutta*), Atlantic salmon (*Salmo salar*) and Euroasian
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20 110 minnow (*Phoxinus phoxinus*), successful passages occurred for a 1.25 ratio, while Lauritzen
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22 111 et al. (2005), for sockeye salmon (*Oncorhynchus nerka*), reported successes in ratios ranging
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24 112 from 0.68 to 1.53. On the other hand, Ovidio and Philippart (2002) assessed the impact of 28
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26 113 small weirs on the upstream movements of six fish species, and focused on the need of a
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28 114 minimum plunge pool depth for a successful negotiation, postulating that water depth
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30 115 downstream of the obstacle should be at least “twice the size of the fish”. Kondratieff and
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32 116 Myrick (2006), and more recently Ficke et al. (2011) also highlighted the importance of
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34 117 plunge pool depth suggesting a minimum threshold not lower than 10 cm, to avoid inhibition
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36 118 of fish movements and minimize predation risk. It is clear that the effect of both plunge pool
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38 119 depth and waterfall height on upstream fish movements needs to be further addressed to
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40 120 quantify fish jumping performance and thus set guidelines for appropriate fish passage
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42 121 designs. This is particularly important for cyprinid fishes that are by far the dominant group of
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44 122 autochthonous freshwater fish in the Iberian Peninsula, and for which performance
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46 123 effectiveness in negotiating small weirs is virtually unknown.

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48 124 The goal of this study is to evaluate the performance of upstream fish movements over
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50 125 a small experimental broad-crested weir adjustable for different plunge pool depths (D) and
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52 126 waterfall heights (Δh), under different flow discharges (Q). The conditions tested are
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3 127 representative of those that fish are expected to overcome when migrating upstream to spawn.
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5 128 Iberian barbel (*Luciobarbus bocagei*) was selected as the target-species, since it is considered
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7 129 representative of at least 8 species of medium-sized benthic potamodromous cyprinids in
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9 130 Iberia and Western Europe, counting the genera *Barbus* and *Luciobarbus* (Santos et al. 2014).
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11 131 It was hypothesized that passage success would increase with decreasing waterfall heights in
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13 132 association with increasing plunge pool depths and low flow discharges.
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19 134 **Material and Methods**

20 135 *Fish and Experimental Facility*

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22 136 Adult Iberian barbel used in the experiments (n = 380; mean total length (TL) \pm standard
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24 137 deviation (SD) = 18.7 \pm 3.3 cm) were captured in the Lisandro River, a small Atlantic coastal
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26 138 river. Sampling was performed by wadable electrofishing (Hans Grassl IG-200) according to
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28 139 the protocol adopted by the European Committee for Standardization (CEN 2003). Six
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30 140 electrofishing episodes were performed (one episode per week), collecting 65 fish per
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32 141 episode. Fish were transported to the laboratory facilities, at the Hydraulics and Environment
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34 142 Department of the National Laboratory for Civil Engineering (LNEC), in a fish transport box
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36 143 (Hans Grassl, 190 L) with external aeration. At LNEC, fish were maintained for a maximum
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38 144 period of six days in filtered and aerated acclimation tanks (700 L tanks; Fluval Canister
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40 145 Filter FX5). To ensure high water quality levels in the acclimation tanks, water temperature
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42 146 (22 °C \pm 1 °C), pH (\approx 7.3) and conductivity (215 \pm 37 $\mu\text{s}\cdot\text{cm}^{-1}$) were monitored every day
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44 147 using a multiparametric probe (HANNA, HI 9812-5). Water replacement was performed daily
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46 148 with a turnover rate of 150 L $\cdot\text{day}^{-1}$. Feeding (Tetra Pond sticks) stopped 24–48 h prior to the
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48 149 experiments.
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54 150 Experiments were conducted in an indoor experimental ecohydraulic channel installed
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56 151 at LNEC. The channel (Figure 1A) consists of a rectangular steel frame (10.0 m long x 1.0 m
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3 152 wide x 1.2 m high) with glass-viewing panels on sidewalls that allow free observation of fish
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5 153 within the flume. The facility includes an upstream and a downstream tank, separated from
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7 154 the flume by mesh panels, from where the water enters the flume and is recirculated. The
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9 155 channel was tilted at a 3% slope, determined to be representative of central and southern
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11 156 Iberian rivers according to the European River and Catchment Database (Catchment
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13 157 Characterisation and Modelling, version 2 [CCM2]; Vogt et al. 2007). Water quality in the
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15 158 flume was also monitored after each experiment. No difference was registered between water
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17 159 temperature in acclimation tanks and in the flume ($22\text{ }^{\circ}\text{C} \pm 1\text{ }^{\circ}\text{C}$); values of pH and
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19 160 conductivity were of ≈ 8.3 and $172 \pm 22\text{ }\mu\text{s}\cdot\text{cm}^{-1}$, respectively.
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162 ***Testing Plunge Pool Depths and Waterfall Heights***

163 To study the effects of plunge pool depths and waterfall heights on upstream passage of
164 Iberian barbel, an experimental broad-crested weir made of polyvinyl chloride (PVC)
165 modules was tested for a factorial design of 16 combinations (Table 1) considering four
166 different plunge pool depths ($D = 10, 20, 30, 50\text{ cm}$), and four waterfall heights ($\Delta h = 5, 10,$
167 $15, 25\text{ cm}$). Minimum plunge pool depth was difficult to setup because it depends on the size
168 and swimming capabilities of fish, and how the plunging jet dissipates downstream of the
169 weir (Baudoin et al. 2014). Nonetheless, for large rheophilic cyprinids, these authors propose
170 a water depth of 10 cm as the minimum to overcome an obstacle, which was therefore the
171 threshold selected for the present study. Maximum waterfall height for the current
172 experiments was determined by carrying out preliminary studies. A lower waterfall height (5
173 cm) was used initially and, in subsequent trials, fish were presented with increasing heights (5
174 cm increments) until no fish could negotiate the weir. This final height was taken to be the
175 critical weir height. The maximum waterfall height used in the trials was the critical weir

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3 176 height plus 5 cm. Once the maximum waterfall height was determined, trials were assigned
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5 177 randomly, resulting in ratios of $D/\Delta h$ that ranged from 0.4 to 10.
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7 178 The experimental weir (Figure 1B) spanned the entire channel width, with a constant
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9 179 thickness of 20 cm, and it was installed in the flume at 2.75 m upstream of the acclimation
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11 180 area, which was created in the downstream zone of the flume by two mesh panels 1 m apart.
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13 181 Immediately downstream of the weir, a 0.65 m long zone was considered as the approach
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15 182 area. Flow discharge was measured by a flow meter installed in the supply pipe and
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17 183 maintained equal to $50 \text{ L}\cdot\text{s}^{-1}$. The different waterfall heights (Figure 1C) were setup by adding
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19 184 or removing modules from the weir. The plunge pool depth below the weir was controlled by
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21 185 a gate located at the downstream tank of the channel.
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25 186 Before each trial, fish were held 15 minutes in the acclimation area to allow adaptation
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27 187 to the flume conditions. After that period, the upstream mesh panel was removed and fish
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29 188 were allowed to volitionally explore the channel for 60 minutes. Both upstream and
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31 189 downstream passage was allowed, so fish could negotiate the weir multiple times. Each
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33 190 combination tested had 4 replicates carried out with schools of 5 fish for each replica. Each
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35 191 fish was used only once and was randomly selected. Fish movements were monitored by
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37 192 direct observation and recorded by a video camera (GoPro HERO3). Registered observations
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39 193 included: number of fish that approached the weir (A_p ; fish that entered the approach area),
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41 194 number of passage attempts (A_t ; fish that actively tried to negotiate the waterfall), number of
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43 195 passage successes (N), and time taken to achieve the first successful upstream passage (T ;
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45 196 min). At the end of each trial, fish were measured ($TL \pm 0.1 \text{ cm}$) and water temperature and
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47 197 quality (pH and conductivity) in the flume were monitored. All trials were performed during
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49 198 late spring and early summer, in the morning period (07–13h) so that environmental
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51 199 conditions, such as temperature and light, were fairly constant throughout the experiments.
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3 201 ***Effects of Flow Discharge on Upstream Movement of Fish***
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5 202 To study the effects of flow discharge on barbel capacity to successfully negotiate a small
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7 203 weir, 3 additional discharges were tested: 25, 75 and 100 L.s⁻¹. These discharges were tested
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9 204 with the combination of waterfall height and plunge pool depth that previously showed the
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11 205 highest passage success with 50 L.s⁻¹ and also followed the procedures previously described.
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16 207 ***Hydrodynamics Characterization***
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18 208 To characterize the hydrodynamic conditions downstream of the weir, the 3 components of
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20 209 flow velocity (x, y, z) were measured with a downward-looking 3D Acoustic Doppler
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22 210 Velocimeter (Vectrino ADV; Nortek AS). A grid with 27 sampling points was implemented
23
24 211 at the centre of the flume, assuming flow symmetry across its width. The sampling points
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26 212 were established according to the expected velocity field variation and taking into account the
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28 213 limitations of the ADV equipment. Such limitations included the minimum distance required
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30 214 at the bottom of the flume (5 cm) and near the obstacle, as well as the need for the probe to be
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32 215 completely immersed during the data acquisition period. This was difficult to ensure near the
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34 216 weir for some combinations due to turbulence derived from the energy dissipation of the
35
36 217 plunging jet downstream the weir. Water velocity data were acquired at a sampling rate of 25
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38 218 Hz for a period of 180 s. The combinations characterized were: the one that registered a lower
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40 219 passage success; the combination expected to achieve the best passage results; and the
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42 220 combination that actually provided the best results.
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50 222 ***Data Analysis***
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52 223 In order to determine the potential negotiation of the weir for the combinations tested,
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54 224 similarly to studies on efficiency of fishways (Bunt et al. 1999; Lucas and Baras 2001;
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225 Aarestrup et al. 2003; Calles and Greenberg 2009), the percentage of attraction efficiency
 226 (AE) and passage efficiency (PE) were calculated from equations 1 and 2.

$$228 \quad AE \% = 100 \times \frac{\text{number of fish that attempted to negotiate the weir}}{\text{number of fish that entered the approach area}} \quad (1)$$

$$230 \quad PE \% = 100 \times \frac{\text{number of successful passages}}{\text{number of fish that attempted to negotiate the weir}} \quad (2)$$

232 To determine the influence of plunge pool depths, waterfall heights and their
 233 interaction ($D \times \Delta h$) on the number of successful upstream passages of Iberian barbel, a
 234 distance-based MANOVA (PerMANOVA) using the Euclidean distance was performed by
 235 using PC-ORD 6 (Peck, 2010). Likewise, to test the effect of flow discharge on the successful
 236 negotiation of the weir a Kruskal–Wallis ANOVA with a post hoc Dunn’s test for pairwise
 237 comparison was performed by using the *dunn.test* package (Dinno 2015) from the open-
 238 source software R (R Core Team 2014).

239 Data on instantaneous velocity (V_i) were filtered with WinADV freeware software
 240 (Wahl 2001) using the Goring and Nikora (2002) phase-space threshold despiking method,
 241 modified by Wahl (2003). Then, to analyse velocity fluctuations and turbulence gradients
 242 along the water column in a vertical plane, the resultant V_{xz} and turbulent kinetic energy
 243 (TKE; important turbulence descriptor (Wang et al. 2011; Wilkes et al. 2013) in ecohydraulic
 244 studies) were calculated and represented graphically, by vector and contour maps, in order to
 245 illustrate the hydrodynamic conditions within the test area (*e.g.* areas of high velocity and
 246 turbulence gradients) that might have affected fish movements. Additionally, for the tested
 247 discharges, differences in flow velocities and turbulence were analysed using a non-
 248 parametric Friedman test followed by a Nemenyi post hoc test applying the R package
 249 *PMCMR* (Pohlert 2015).

250

251 **Results**252 *Plunge Pool Depths and Waterfall Heights*

253 Fish attempted to negotiate all $D \times \Delta h$ tested combinations (Table 2) (an example of a
254 successful attempt is illustrated in Figure 1C). However, successful upstream passage as well
255 as the number of fish approaches, the number of attempts to pass the weir, and the time
256 needed to successfully pass upstream, were markedly variable among combinations. Overall,
257 a total of 254 upstream successful passages were registered for all combinations of $D \times \Delta h$.
258 Regarding the approach movements and attempts to pass the weir, an average of 710
259 approaches (max = 1013 approaches, in $D50\Delta h15$; min = 293, in $D10\Delta h25$) and 183 attempts
260 (max = 328 attempts, in $D30\Delta h05$; min = 65, in $D10\Delta h05$) were recorded.

261 The best results were achieved for the combination of $D20\Delta h10$ ($D/\Delta h = 2$), with 50
262 successful passages and a PE of 17%. This percentage of PE was only surpassed by
263 combination $D10\Delta h15$ ($D/\Delta h = 0.67$; 20%), however in $D10\Delta h15$ both the number of
264 attempts (90) and the number of successful passages (18) were lower than $D20\Delta h10$.
265 Additionally, combination $D20\Delta h10$ registered the highest percentage of AE (53%), with a
266 total of 548 approaches that resulted in 291 attempt movements. Having the same $D/\Delta h$ ratio
267 as combination $D20\Delta h10$, $D/\Delta h = 2$, combinations $D10\Delta h05$, $D30\Delta h15$ and $D50\Delta h25$
268 however, recorded very different passage successes (10, 9, and 4 upstream passages,
269 respectively) and the percentages of AE and PE were also lower compared with the results of
270 combination $D20\Delta h10$.

271 The poorest results were registered for combination $D10\Delta h25$ ($D/\Delta h = 0.4$), with only
272 1 successful upstream passage and a PE of 1%. This combination registered also the lowest
273 number of approaches, a total of 293, and only 72 attempts. Moreover, it actually registered
274 the highest time until the first (and single one) successful passage occurred (46 min).

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3 275 Combination D50 Δ h05 ($D/\Delta h = 10$), which was expected to provide the best results due to its
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5 276 higher plunge pool depth in association to a lower waterfall height to overcome, only ranked
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7 277 third with 25 successful passages, 27% of AE, and 13% of PE.

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9 278 Results of the PerMANOVA analysis showed significant effects of D ($F = 5.46$; $P =$
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11 279 0.004), Δh ($F = 4.68$; $P = 0.006$), and the interaction $D \times \Delta h$ ($F = 3.02$; $P = 0.005$) on the
12
13 280 number of successful upstream fish passage events. Pairwise comparisons (Table 3)
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15 281 performed for each factor showed that the number of successful fish movements past the weir
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17 282 was significantly different, and higher, for $D = 20$ cm, in relation to the other tested plunge
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19 283 pool depths. On the contrary, for the tested waterfall heights, $\Delta h = 25$ cm was significantly
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21 284 different, registering the lowest number of successful movements.
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26 27 286 *Flow Discharge*

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29 287 The number of successful upstream passages, as well as fish approaches and attempts to pass
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31 288 the weir were found to decrease with the increment of flow discharge (Table 4). The largest
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33 289 number of attempts (total of 291) and successful passages (50) were registered for $50 \text{ L}\cdot\text{s}^{-1}$.
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35 290 On the contrary, the discharge of $100 \text{ L}\cdot\text{s}^{-1}$ proved to be the most limiting for fish, registering
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37 291 only 26 approaches and 12 attempts to negotiate the weir, which resulted in a single
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39 292 successful passage almost at the end of the trial (57 min). For $25 \text{ L}\cdot\text{s}^{-1}$, there were a high
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41 293 number of fish approaches (a total of 1440), but resulted in only 280 attempts leading to a low
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43 294 AE (19%). PE was also low due to the small number of successful passages (14).

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47 295 Results of the Kruskal–Wallis test show that flow discharge significantly affected the
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49 296 number of successful passages of barbel ($H = 10.95$; 3 *df.*; $P = 0.01$). Further, Dunn's
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51 297 multiple comparison test (Table 5) revealed that for $100 \text{ L}\cdot\text{s}^{-1}$, the number of successful
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53 298 passages was significantly lower than for $25 \text{ L}\cdot\text{s}^{-1}$ and especially for $50 \text{ L}\cdot\text{s}^{-1}$. Likewise,
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3 299 successful passages for 75 L.s^{-1} were also significantly lower compared to the ones that
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5 300 occurred for 50 L.s^{-1} .

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8 9 302 ***Hydrodynamics***

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11 303 Figures 2 and 3 display the variation of TKE and flow velocity, respectively, for the different
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13 304 conditions tested. Contour maps revealed that both TKE values (Figure 2A, 2B, 2D, and 2E)
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15 305 and velocity (Figure 3A, 3B, 3D, and 3E) increased with flow discharges. This increase was
16
17 306 particularly important in the case of 75 L.s^{-1} , where values of TKE above $1 \text{ m}^2.\text{s}^{-2}$ and velocity
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19 307 just above 1 m.s^{-1} were registered close to the foot of the weir, and for the 100 L.s^{-1} which
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21 308 also registered similar values, although these were located furthest from the weir. For
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23 309 combinations D20 Δ h05 (Figure 2C and Figure 3C; that registered a lower passage success)
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25 310 and D50 Δ h05 (Figure 2F and Figure 3F; combination that was expected to achieve the best
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27 311 passage results), values of TKE and velocity were slightly higher when compared with
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29 312 D20 Δ h10 (Figure 2B).

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34 313 Statistical analysis of hydraulic characterization of combinations D20 Δ h10, D20 Δ h05,
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36 314 and D50 Δ h05, demonstrate that there were significant differences among their respective V_{xz}
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38 315 ($F_r = 11.76$; 2 *d.f.*; $P < 0.01$) and TKE values ($F_r = 7.44$; 2 *d.f.*; $P < 0.05$). Regarding the flow
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40 316 discharges tested in combination D20 Δ h10, results of Friedman tests revealed that the four
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42 317 flows were significantly different both in terms of velocity ($F_r = 53.73$; 3 *d.f.*; $P < 0.001$) and
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44 318 TKE ($F_r = 78.03$; 3 *d.f.*; $P < 0.001$); nevertheless, results of pairwise comparisons for the
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46 319 parameter velocity show that there were no significant differences for 25 L.s^{-1} vs. 50 L.s^{-1} (P
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48 320 = 0.46).

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52 53 322 **Discussion**

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3 323 This study highlights the importance of plunge pool depth, waterfall height, and flow
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5 324 discharge, as well as their interaction, for the successful negotiation of Iberian barbel over
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7 325 small broad-crested weirs. The high numbers of recorded movements (approaches and
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9 326 attempts) as well as passage successes demonstrated that Iberian barbel were stimulated to
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11 327 move upstream and negotiate the weir. Nevertheless, passage success varied among
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13 328 combinations, indicating that some of the combinations were more favourable for upstream
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15 329 passage as a consequence of suitable hydrodynamic conditions for fish (Liao 2007; Williams
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17 330 et al. 2012; Elder and Coombs 2015).

20 331 Similar to other studies (Kondratieff and Myrick 2005; Brandt et al. 2005; Kondratieff
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22 332 and Myrick 2006; Ficke et al. 2011), results from attraction efficiency, passage efficiency,
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24 333 and passage success recorded for $D \times \Delta h$, demonstrate that the combination of shallow plunge
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26 334 pool depths with high waterfall heights, which produce low $D/\Delta h$ ratios, may inhibit the
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28 335 successful passage of Iberian barbel. Generating such unfavourable conditions, combination
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30 336 $D10\Delta h25$, which matched the smallest $D/\Delta h$ ratio tested ($D/\Delta h = 0.4$), achieved only one
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32 337 successful upstream passage. However, for combination $D10\Delta h15$, the second smallest ratio
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34 338 tested ($D/\Delta h = 0.67$), and similar to the one reported by Lauritzen et al. (2005) as the
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36 339 minimum ratio to allow sockeye salmon to negotiate barriers, the number of passage
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38 340 successes increased to 18. Nevertheless, passage success did not always increase with
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40 341 increasing $D/\Delta h$ ratios – for example, 28 successful passages were recorded for $D/\Delta h = 3$
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42 342 (combination $D30\Delta h10$) and for $D/\Delta h = 6$ (combination $D30\Delta h05$) only 17 successes were
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44 343 achieved. Interestingly, and contrary to what might be expected, combination $D50\Delta h05$,
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46 344 which represented the maximum $D/\Delta h$ ratio tested ($D/\Delta h = 10$), did not register the highest
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48 345 number of passage successes; it ranked only third.

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52 346 Another interesting result was that for combinations with the same $D/\Delta h$ ratio ($D/\Delta h =$
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54 347 2 for $D10\Delta h05$, $D20\Delta h10$, $D30\Delta h15$ and $D50\Delta h25$), different numbers of passage success

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3 348 were recorded ($N = 10, 50, 9,$ and $4,$ respectively). This highlights the fact that, combinations
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5 349 with the same $D/\Delta h$ ratio generate different hydrodynamic patterns bellow the weir, thereby
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7 350 affecting the successful passage of fish over it. These results corroborate what was postulated
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9 351 by Baudoin et al. (2014) about the energy dissipation of the plunging jet downstream of a
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11 352 weir playing an important role on the attraction and, especially, on the passage success of fish.
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13 353 In fact, in combinations tested, values of PE were, in general, lower than AE estimates,
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15 354 pointing out that passage limitations are more severe than attraction limitations. Additionally
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17 355 to the jet energy dissipation, should also be highlighted that the nappe shape, which depends
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19 356 on the specific flow discharge, and the amount of air entrainment also influence the successful
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21 357 negotiation of these obstacles. Furthermore, other aspects not considered in this study, like the
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23 358 plan shape of the weir and the downstream bottom irregularities, which influence the flow
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25 359 field characteristics (Pasternack et al. 2006; Vallé and Pasternack 2006; Wyrick and
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27 360 Pasternack 2008), may also play a role on the fish performance when negotiating small weirs.

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32 361 The importance of jet dissipation, nappe profile and air entrainment were also evident
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34 362 in flow discharge tests implemented for combination $D20\Delta h10$. Fewer approaches, attempts
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36 363 to pass the weir, and successful passages were recorded with increasing flows and, in
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38 364 addition, fish also required more time to negotiate the weir. The highest number of passage
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40 365 successes was not achieved for the lowest discharge ($25 \text{ L}\cdot\text{s}^{-1}$), although an elevated number
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42 366 of fish approaches were recorded, which lead us to surmise that the plunging jet and the nappe
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44 367 formed in the downstream face of the weir (to vertical and shallow) were not sufficiently
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46 368 efficient to form an attractive path (see Powers and Orsborn 1985) to stimulate fish to
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48 369 negotiate the obstacle. On the other hand, for higher discharges (75 and $100 \text{ L}\cdot\text{s}^{-1}$), the TKE
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50 370 values created by the plunging jet were considerably high, with intensities above $1 \text{ m}^2\cdot\text{s}^{-2}$
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52 371 registered close to the weir. High velocities ($> 1 \text{ m}\cdot\text{s}^{-1}$) were also observed which, together
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55 372 with the high TKE and the consequent aeration, may have decreased the ability of fish to
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3 373 negotiate the weir, since cyprinids, like Iberian barbel, are shorter in length and generate
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5 374 lower speeds compared to salmonid species (Doadrio 2001; Silva et al. 2009; Alexandre et al.
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7 375 2013; Katopodis and Gervais 2016).

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10 376 Thus, this study showed that the successful passage of small vertical weirs by cyprinid
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12 377 species is a complex phenomenon where not only the plunge pool depth and waterfall height,
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14 378 which have been studied previously, especially for salmonids, are important, but in addition
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16 379 flow discharge contributes to setting the most favourable hydrodynamic conditions for fish to
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18 380 overcome the obstacle. Some results were different than those which might be expected from
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20 381 more simplistic assumptions, as some of the combinations that might have been predicted to
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22 382 be easily negotiated by fish turned out to be more difficult, leading to lower success of
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24 383 passage. This highlights the complexity and importance of the interaction of geometry and
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26 384 hydraulic parameters, as well as fish abilities, to achieve successful negotiation of small
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28 385 obstacles. Although defining $D/\Delta h$ thresholds for successful fish negotiation is important,
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30 386 both nominal values of each parameter should also be taken into account when designing or
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32 387 retrofitting weir-like structures, otherwise their impact on river functional connectivity will
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34 388 not be improved as might be expected.

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38 389 In nature, all the unfavourable conditions experienced in this study (shallow plunge
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40 390 pool depths, high waterfall heights, low flow discharges, high turbulence and air entrainment)
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42 391 commonly occur. These may lead to an increase in energy expenditures of fish during
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44 392 negotiation of the obstacles (Enders et al. 2005; Tritico and Cotel 2010) that may then reduce
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46 393 swimming performance and possibly cause disorientation (Pavlov et al. 2000; Liao 2007;
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48 394 Tritico and Cotel 2010) and fish fatigue (Katopodis and Gervais 2012). All these conditions
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50 395 may delay fish migration and/or reduce the number of fish that access important upstream
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52 396 habitats for spawning (in addition to other adverse effects; e.g. Ovidio and Philippart 2002;
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54 397 Castro-Santos and Haro 2003; Kemp and O'Hanley 2010; McLaughlin et al. 2013).

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3 398 The outcomes of this work are expected to be useful to identify potential migration
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5 399 obstacles for potamodromous cyprinids and to define design criteria for the requalification of
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7 400 small barriers (Ovidio and Philippart 2002; Kondratieff and Myrick 2006) improving fish
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9 401 passage and consequently habitat connectivity, and population management (Meixler et al.
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11 402 2009). Being a laboratory based study, it is recognised that the tested parameters and their
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13 403 respective interactions do not fully explain all the complex situations that fish can encounter
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15 404 in nature (e.g. temperature, noise, substrate roughness, weir geometry irregularities, channel
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17 405 complexity, cover, etc.). Furthermore, not all size classes of fish were tested, due to the
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19 406 burden that these experiments would represent (time, number of fish, laboratory conditions),
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21 407 and so, different behaviours and abilities may be expected in experiments, and in the field,
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23 408 with other size classes. However, fish used in the experiments were chosen within the range
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25 409 of 15–25 cm total length that represents the typical size class of natural adult fish, the most
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27 410 active size class in upstream migration of this and other medium-sized benthic
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29 411 potamodromous cyprinids found in Iberian and European river ecosystems (Doadrio et al.,
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31 412 2011; Kottelat and Freyhof, 2007). Nevertheless, this work provided valuable insights that, in
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33 413 future researchs, should definitely combine lab and *in situ* studies (Lauritzen et al. 2005;
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35 414 Pasternack et al. 2006; Ovidio et al. 2007; Kemp et al. 2011) to better understand how fish
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37 415 species respond to macro- and micro-hydrodynamic complex conditions downstream of
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39 416 barriers, what attracts them and what repels them. This is the key to enhance knowledge on
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41 417 negotiation of small instream obstacles by fish and to develop and design successful passage
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43 418 facilities (Williams et al. 2012).

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52 **Acknowledgments**

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55 421 This research was financially supported by the Foundation for Science and Technology (FCT) through
56
57 422 the project FISHMOVE (PTDC/AGR-CFL/117761/2010). Susana D. Amaral was funded by a PhD
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3 423 grant from University of Lisbon/Santander Totta (SantTotta/BD/RG2/SA/2011), and by FCT
4
5 424 (SFRH/BD/110562/2015). Paulo Branco was financed by a grant from FCT
6
7 425 (SFRH/BPD/94686/2013). Ana T. Silva was financed by the SafePass project (no. 244022) funded by
8
9 426 the Research Council of Norway (RCN) under the ENERGIX program. The authors would like to
10
11 427 thank the staff of the National Laboratory for Civil Engineering (LNEC) for all the support during the
12
13 428 experiments. Thanks are also extended to Prof. Gregory Pasternack and two anonymous reviewers, for
14
15 429 their helpful comments on an early draft of this manuscript. Fishing and handling permits for capture
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17 430 fish in the field were issued by the Institute for Nature Conservation and Forests (ICNF) (permit
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19 431 number 23/2014/CAPT, 24/2014/CAPT and 25/2014/CAPT).
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Table 1 – Tested plunge pool depths and waterfall heights ($D \times \Delta h$) in the experimental weir to assess upstream passage performance of Iberian barbel.

		Waterfall heights (cm) – Δh			
		$\Delta h05$	$\Delta h10$	$\Delta h15$	$\Delta h25$
Plunge pool depths (cm) – D	D10	D10 $\Delta h05$	D10 $\Delta h10$	D10 $\Delta h15$	D10 $\Delta h25$
	D20	D20 $\Delta h05$	D20 $\Delta h10$	D20 $\Delta h15$	D20 $\Delta h25$
	D30	D30 $\Delta h05$	D30 $\Delta h10$	D30 $\Delta h15$	D30 $\Delta h25$
	D50	D50 $\Delta h05$	D50 $\Delta h10$	D50 $\Delta h15$	D50 $\Delta h25$

Table 2 – Results of the combinations of plunge pool depths and waterfall heights tested ($D \times \Delta h$). $D/\Delta h$, plunge pool depth/ waterfall height ratio; Q , flow discharge ($L \cdot s^{-1}$); n , number of fish tested; A_p , total number of approaches; A_t , total number of attempts to pass the weir; N , total number of successful passages; % AE, percentage of attraction efficiency (ratio of the number of attempts per number of approaches $\times 100$); %PE, percentage of passage efficiency (ratio of successful passages per number of attempts $\times 100$); T , mean time until the first successful passage (min).

$D \times \Delta h$	$D/\Delta h$	Q	n	A_p	A_t	N	%AE	%PE	T
D10 Δ h05	2	50	20	774	65	10	8	15	33
D10 Δ h10	1	50	20	733	138	11	19	8	29
D10 Δ h15	0.67	50	20	765	90	18	12	20	15
D10 Δ h25	0.40	50	20	293	72	1	25	1	46
D20 Δ h05	4	50	20	687	183	9	27	5	22
D20 Δ h10	2	50	20	548	291	50	53	17	15
D20 Δ h15	1.33	50	20	943	248	24	26	10	17
D20 Δ h25	0.80	50	20	746	173	19	23	11	33
D30 Δ h05	6	50	20	682	328	17	48	5	15
D30 Δ h10	3	50	20	650	299	28	46	9	24
D30 Δ h15	2	50	20	525	204	9	39	4	24
D30 Δ h25	1.20	50	20	715	110	3	15	3	13
D50 Δ h05	10	50	20	734	196	25	27	13	24
D50 Δ h10	5	50	20	676	146	8	22	5	20
D50 Δ h15	3.33	50	20	1013	171	18	17	11	9
D50 Δ h25	2	50	20	885	210	4	24	2	26

Table 3 – Results of the pairwise comparisons, after the main test (PerMANOVA), on the number of successful fish movements for factors: **A)** plunge pool depths (D), and **B)** waterfall height (Δh). Bold values highlight significant differences..

Factor	Pairwise comparisons	Results	
		<i>t</i>	<i>P</i>
D	D10 vs. D20	3.05	<0.01
	D10 vs. D30	1.73	0.094
	D10 vs. D50	1.34	0.197
	D20 vs. D30	2.05	<0.05
	D20 vs. D50	2.07	0.05
	D30 vs. D50	0.14	0.871
Δh	$\Delta h05$ vs. $\Delta h10$	1.88	0.070
	$\Delta h05$ vs. $\Delta h15$	0.55	0.572
	$\Delta h05$ vs. $\Delta h25$	2.63	<0.05
	$\Delta h10$ vs. $\Delta h15$	1.32	0.192
	$\Delta h10$ vs. $\Delta h25$	3.47	<0.01
	$\Delta h15$ vs. $\Delta h25$	2.67	<0.05

$\alpha = 0.05$

Table 4 – Results of the experimental designs to test the influence of flow discharge on the jumping performance of Iberian barbel. $D \times \Delta h$, tested combination; Q , flow discharge ($L \cdot s^{-1}$); n , number of fish tested; A_p , total number of approaches; A_t , total number of attempts to pass the weir; N , total number of successful passages; % AE, percentage of attraction efficiency (ratio of the number of attempts per number of approaches $\times 100$); %PE, percentage of passage efficiency (ratio of successful passages per number of attempts $\times 100$); T , mean time until the first successful passage (min).

$D \times \Delta h$	Q	n	A_p	A_t	N	%AE	%PE	T
D20 Δ h10	25	20	1440	280	14	19	5	27
	50	20	548	291	50	53	17	15
	75	20	208	66	8	32	12	40
	100	20	26	12	1	46	8	57

Note: Results from $Q = 50 L \cdot s^{-1}$ are the same presented in Table 1. They are presented here for ease of comparison.

Table 5 – Results of the pairwise comparisons (Dunn’s post-hoc test), after the main test (Kruskal–Wallis), on the number of successful fish movements for factor flow discharge (Q). Bold values represent significant differences.

Factor	Pairwise comparisons	Results	
		<i>Z</i>	<i>P</i>
Q	Q25 vs. Q50	1.20	0.11
	Q25 vs. Q75	-0.86	0.19
	Q25 vs. Q100	-1.99	0.02
	Q50 vs. Q75	-2.07	0.02
	Q50 vs. Q100	-3.19	<0.001
	Q75 vs. Q100	-1.13	0.13

$\alpha = 0.05$

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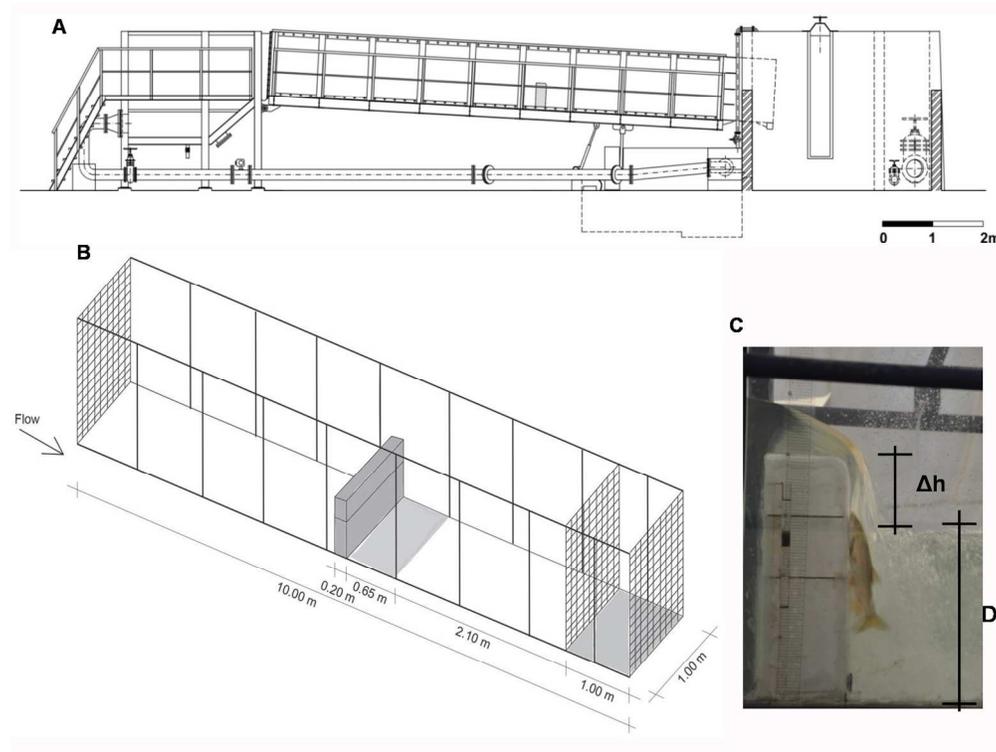


Figure 1 – Representation of: A) side view of the experimental channel on a slope of 3%; B) three dimensional scheme of the experimental ecohydraulic flume showing the location of the experimental weir (2.75 m upstream the acclimation area), the acclimation area (1 m² area shown shaded between the two removable fine mesh panels located downstream), and the approach area (0.65 m² shaded area immediately downstream the weir); and C) experimental design considering the plunge pool depth (D - distance from the bottom of the flume to the top of the water surface) and waterfall height (Δh - distance from the water surface to the top of the crest of the experimental weir). This picture provides a visible attempt by fish to swim up the skimming flow formed in the downstream face of the weir.

542x410mm (96 x 96 DPI)

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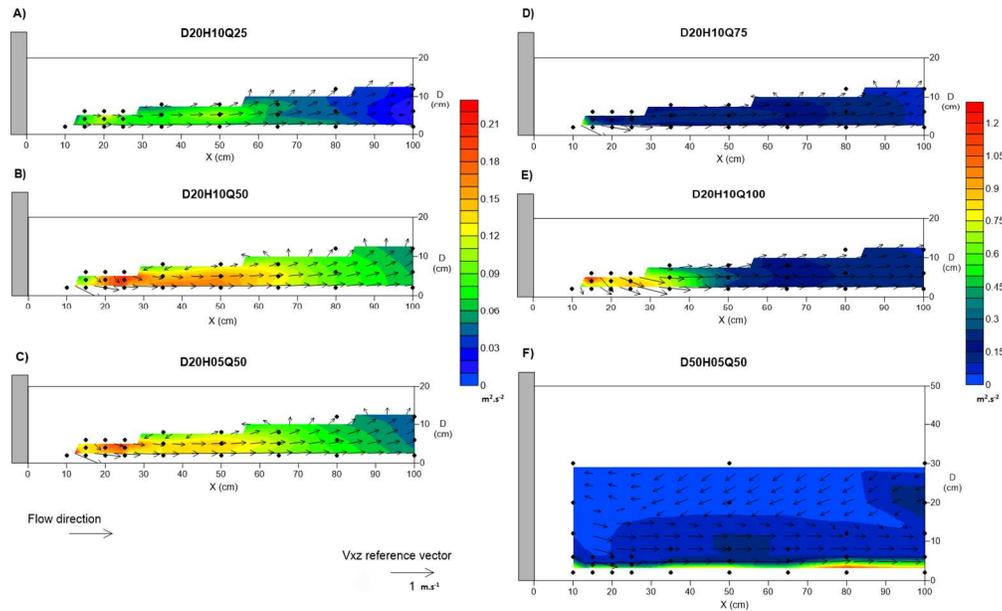


Figure 2 – Graphical representation of turbulent kinetic energy (TKE; $\text{m}^2.\text{s}^{-2}$) and velocity vectors (V_{xz} ; $\text{m}.\text{s}^{-1}$) for combinations tested: A) D20 Δ h10 with 25 $\text{L}.\text{s}^{-1}$; B) D20 Δ h10 with 50 $\text{L}.\text{s}^{-1}$; C) D20 Δ h05 with 50 $\text{L}.\text{s}^{-1}$; D) D20 Δ h10 with 75 $\text{L}.\text{s}^{-1}$; E) D20 Δ h10 with 100 $\text{L}.\text{s}^{-1}$; and F) D50 Δ h05 with 50 $\text{L}.\text{s}^{-1}$. X is the distance from the weir (cm) and D is the water depth (cm). Points represent the measuring mesh.

294x178mm (145 x 145 DPI)

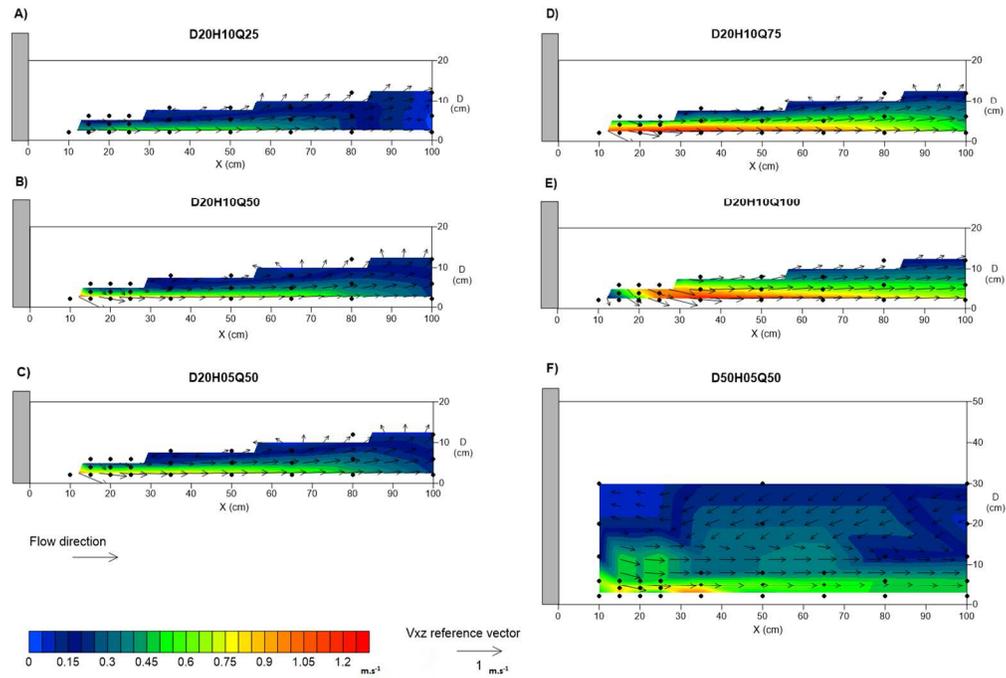


Figure 3 – Magnitude and direction of water velocity (V_{xz} ; $\text{m}\cdot\text{s}^{-1}$) in combinations tested: A) D20 Δ h10 with $25 \text{ L}\cdot\text{s}^{-1}$; B) D20 Δ h10 with $50 \text{ L}\cdot\text{s}^{-1}$; C) D20 Δ h05 with $50 \text{ L}\cdot\text{s}^{-1}$; D) D20 Δ h10 with $75 \text{ L}\cdot\text{s}^{-1}$; E) D20 Δ h10 with $100 \text{ L}\cdot\text{s}^{-1}$; and F) D50 Δ h05 with $50 \text{ L}\cdot\text{s}^{-1}$. X is the distance from the weir (cm) and D is the water depth (cm). Points represent the measuring mesh.

282x191mm (144 x 144 DPI)